

CORRIGENDUM / RECTIFICATIF

Corrigendum: Strength mobilization in clays and silts

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On page 1497, eqs. [24], [26], and [28] should read:

$$[24] \quad \frac{q}{6c_u} = \frac{1}{2} \left(\frac{1.35w}{\gamma_{M=2} D} \right)^{0.6}$$

$$[26] \quad \frac{w}{D} = 2.35 \left(\frac{\gamma_{M=2}}{M^{1.67}} \right)$$

$$[28] \quad \frac{w}{D} = 0.74 \gamma_{M=2}$$

The range of settlements implied by the range of $M = 2$ in the database (shown in Fig. 10) is calculated as 2.2 to 65.1 mm. At the upper end of this range there would be serviceability concerns for most structures.

Increasing M to 3.5 reduces this range to 0.9–25.5 mm. The upper end of this range roughly corresponds to an upper limit on tolerable settlements.

This further underlines the finding of the paper that a large mobilization factor is needed for settlement control if no knowledge of soil stress–strain behaviour is considered.

The authors apologise to the readers of *Canadian Geotechnical Journal* for these mistakes in the original paper.

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