Corrigendum: Strength mobilization in clays and silts

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On page 1497, eqs. [24], [26], and [28] should read:

\[ \frac{q}{6c_u} = \frac{1}{2} \left( \frac{1.35w}{\gamma_{M=2} D} \right)^{0.6} \]

\[ \frac{w}{D} = 2.35 \left( \frac{\gamma_{M=2}}{M^{1.67}} \right) \]

\[ \frac{w}{D} = 0.74 \gamma_{M=2} \]

The range of settlements implied by the range of \( M = 2 \) in the database (shown in Fig. 10) is calculated as 2.2 to 65.1 mm. At the upper end of this range there would be serviceability concerns for most structures.

Increasing \( M \) to 3.5 reduces this range to 0.9–25.5 mm. The upper end of this range roughly corresponds to an upper limit on tolerable settlements.

This further underlines the finding of the paper that a large mobilization factor is needed for settlement control if no knowledge of soil stress–strain behaviour is considered.

The authors apologise to the readers of Canadian Geotechnical Journal for these mistakes in the original paper.

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